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低温冻结石门揭煤煤体温度及力学性能变化规律研究

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摘要:为研究低温冻结石门揭煤煤体温度及力学性能变化规律,制作煤样时将U形铜管预埋在煤体内并进行注液氮冻结,通过温度测量、红外热成像、单轴压缩等试验分析了不同冻结时间下煤样内部及表面温度和应力-应变变化特征。试验结果表明:随着冻结时间的增加,煤样内部及表面温度呈下降趋势;煤样表面最低温度位于U形铜管附近,煤样表面最高温度位于煤样边界;在压密阶段,随着冻结时间的增加,煤样应变逐渐减小,压密阶段缩短;在弹性变形阶段和屈服阶段,随着冻结时间的增加,煤样最大应力和弹性模量均呈增大趋势。

关键词:石门揭煤;煤与瓦斯突出;低温冻结;煤体温度;煤体力学性能

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Study on the change law of temperature and mechanical properties of coal body in uncovering coal seam in low temperature freezing cross-cut

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Abstract: In order to study the change law of temperature and mechanical properties of coal body in uncovering coal seam in low-temperature freezing cross-cut, U-shaped copper tubes are pre-buried and frozen with liquid nitrogen during the preparation of coal samples. The characteristics of internal and surface temperature and stress-strain changes of coal samples under different freezing times are analyzed by temperature measurement, infrared thermal imaging and uniaxial compression. The test results show that with the increase of freezing time, the internal and surface temperatures of coal samples show a decreasing trend. The lowest surface temperature of coal samples is located near the U-shaped copper tube, and the highest surface temperature of coal samples is located at the boundary of coal samples. In the compaction stage, with the increase of freezing time, the strain of coal samples gradually decreases and the compaction stage shortens. In the elastic deformation stage and yield stage, with the increase of freezing time, the maximum stress and elastic modulus of coal samples both increase.

Key words: uncovering coal seam in cross-cut; coal and gas outburst; low temperature freezing; coal body temperature; coal body mechanical properties

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0 引言

石门揭煤是我国煤矿井下重要的巷道掘进工程之一。石门揭煤时煤与瓦斯突出强度大,且 80% 以上的特大型煤与瓦斯突出均发生在石门揭煤过程,对煤矿造成严重破坏^[1-2]。根据煤与瓦斯突出机理,煤体的力学强度是决定石门揭煤时能否抵挡煤与瓦斯突出动力的主要因素^[3-4]。因此,为降低石门揭煤过程中煤与瓦斯突出危险性,结合人工冻结技术,国内外学者提出低温冻结石门揭煤方法^[5-6]。在低温冻结作用下,煤体内部孔隙、裂隙中的水冻结成冰,冰的胶结作用可增强煤体的黏聚力,从而提高煤体的力学强度,使煤体状态更加稳定^[7]。叶青等^[8]提出了采用注液冻结技术增强石门揭煤煤体的强度、增加集中应力区和卸压区的长度来防止煤体发生流变而导致煤与瓦斯延时突出;冯涛等^[9-10]通过冻结成型煤样力学实验论证了注液冻结法作为石门揭煤防突方法的可行性;谢雄刚等^[11-12]采用 RFPA^{2D} 系统和 ANSYS 数值模拟软件,分别建立了石门揭煤冻结煤层过程气固耦合数学模型及温度场数值模拟计算模型;翟成等^[13]探究了低温冻结石门揭煤过程中煤体未冻水含量的变化规律。笔者通过试验研究了低温冻结石门揭煤煤体温度及力学性能变化规律,对低温冻结石门揭煤方法的工程实践具有一定的指导作用。

1 试验方案

1.1 煤样制备

试验采用型煤代替原煤,将煤粉、水泥、石膏、黄沙按配比 1:2:2:1 混合并加入适量的水搅拌均匀后倒入立方体模具,待浆液成型后进行脱模,制作 5 个 100 mm×100 mm×100 mm 的煤样。由于铜的导热性能良好,热传导速率快,所以使用 U 形铜管作为导热介质,使液氮从 U 形铜管一端注入,液氮通过 U 形铜管有效吸收煤样中的热量,汽化产生的氮气从 U 形铜管另一端排出。4 个煤样预埋 U 形铜管,煤样通过 U 形铜管持续向液氮放出热量,从而使煤样逐渐被冻结;1 个煤样不预埋 U 形铜管作为对比试验组。通过真空加压饱水装置、电热鼓风干燥箱和电子天平控制煤样含水率为 7%~9%^[14-16],以便对煤样进行冻结。

1.2 试验步骤

(1) 将 4 个预埋 U 形铜管煤样的 U 形铜管与液氮罐通过管阀相连,拧开液氮罐阀门对 U 形铜管注入液氮使煤样分别冻结 15, 30, 45, 60 min。在 U 形铜管垂直平分线上距煤样边缘 1/4 处插入热电

偶,再将热电偶与温度传感器相连,通过温度传感器测量煤样内部温度。液氮温度为-196℃,与煤样的温度差远大于煤样与周围环境之间的温度差,因此热交换主要发生在液氮与煤样之间,且注液氮冻结前在煤壁贴上保温棉,煤样与周围环境的热交换可忽略不计。

(2) 用红外热成像仪测量未预埋 U 形铜管煤样及冻结后煤样的表面温度。

(3) 在煤样侧面沿横向、纵向贴上应变片,将应变片与应变仪相连,在 MTS 电液伺服万能试验机上进行单轴压缩试验(设轴向位移速率为 0.1 mm/min),测量煤样单轴压缩过程产生的应力应变。

试验过程如图 1 所示。

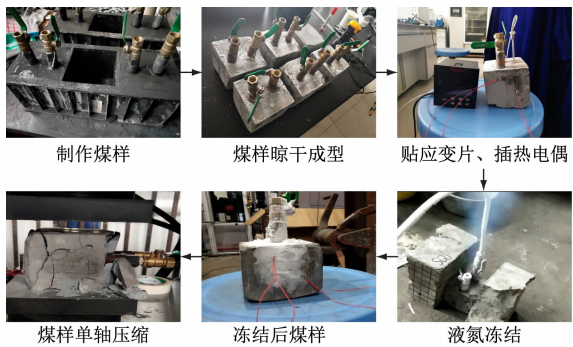


图 1 试验过程

Fig. 1 Experiment process

2 试验结果及分析

2.1 煤样温度变化

不同冻结时间下煤样内部温度变化曲线如图 2 所示,结果见表 1。

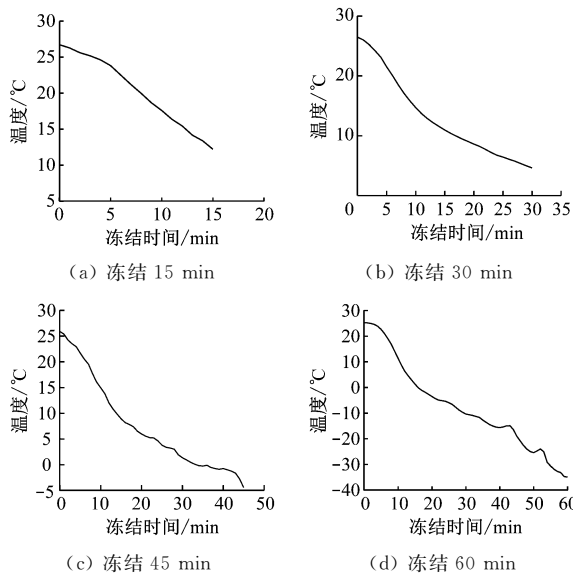


图 2 不同冻结时间下煤样内部温度变化曲线

Fig. 2 Internal temperature variation curves of coal samples under different freezing time

表 1 不同冻结时间下煤样内部温度

Table 1 Internal temperature of coal samples under different freezing time

冻结时间/min	起始温度/℃	冻结后温度/℃	温度降低量/℃
15	26.74	12.21	14.53
30	26.47	4.63	21.84
45	25.89	-4.43	30.32
60	25.33	-34.95	60.28

可看出冻结过程中煤样内部温度持续降低,即冻结时间越长,煤样内部温度降低量越大;冻结 60 min 时,煤样内部温度由 25.33℃降低到-34.95℃,温度降低量达 60.28℃,冻结效果较好。

不同冻结时间下煤样表面温度变化云图如图 3 所示。从图 3 可看出:① 原始煤样表面几何中心温度为 23.45℃,冻结 15,30,45,60 min 后,表面几何

中心温度依次为 10.28,10.07,5.38,-7.30℃;原始煤样表面最低温度为 22.02℃,冻结 15,30,45,60 min 后,表面最低温度依次为 8.01,7.71,4.11,-10.10℃;原始煤样表面最高温度为 24.16℃,冻结 15,30,45,60 min 后,表面最高温度依次为 16.53,14.31,16.86,8.42℃;原始煤样表面平均温度为 23.36℃,冻结 15,30,45,60 min 后,表面平均温度依次为 12.05,10.92,8.60,-1.67℃。这表明随着冻结时间的增加,煤样表面几何中心温度、表面最低温度、表面最高温度和表面平均温度均呈下降趋势。② 煤样表面最低温度位于 U 形铜管附近,煤样表面最高温度位于煤样边界。这是由于液氮与煤样内部的热交换以 U 形铜管为中心逐渐向四周扩散,U 形铜管附近煤的热量最先被液氮吸收,处于煤样边界煤的热量最后被液氮吸收。

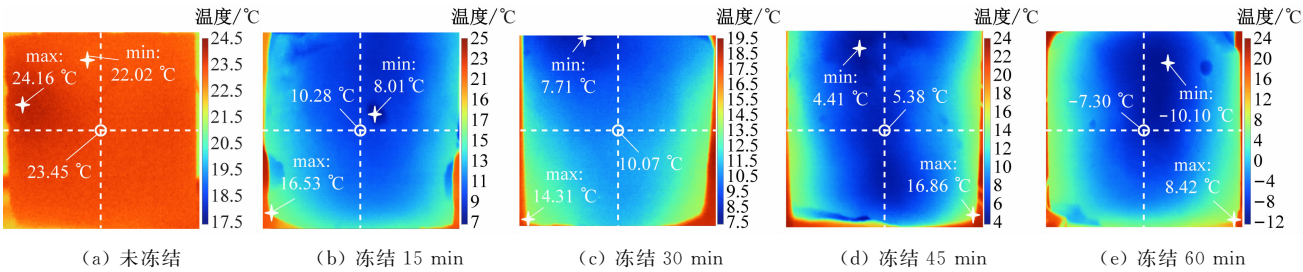


图 3 不同冻结时间下煤样表面温度变化云图

Fig. 3 Surface temperature variation nephogram of coal samples under different freezing time

2.2 煤样力学性能变化

不同冻结时间下煤样应力-应变曲线如图 4 所示,煤体在整个单轴压缩过程中依次经历压密、弹性变形、屈服和破坏 4 个阶段^[17-18]。从图 4 可看出,压密阶段随着冻结时间的增加而缩短,未进行冻结的煤样在压密阶段应变达 1.655 4%,冻结 15,30,45,60 min 的煤样在压密阶段应变分别降到了 0.932 8%,0.388 0%,0.170 8%,0.271 6%,这是由于冻结作用使煤孔隙中的水凝固成冰,压密阶段

应变减小;在弹性变形阶段和屈服阶段,煤样的最大应力随着冻结时间的增加而增大,这是由于煤样内部的水冻结成冰,冰对煤样内部基质颗粒的胶结作用和孔隙的充填作用明显,并且冻结时间越长,煤样冻结程度越高,提高了煤样的力学强度。

不同冻结时间下煤样最大应力和弹性模量见表 2,并采用多项式拟合方式绘制曲线,如图 5 所示。可看出随着冻结时间的增加,煤样的最大应力和弹性模量均呈增大趋势;冻结 60 min 后,最大应力由 2.074 MPa 增大到 4.252 MPa,增幅为 105%,弹性模量由 0.403 GPa 增大到 0.621 GPa,增幅为 54.1%。

表 2 不同冻结时间下煤样最大应力和弹性模量

Table 2 Maximum stress and elastic modulus of coal samples under different freezing time

冻结时间/ min	最大应力/ MPa	最大应力 增幅/%	弹性模量/ GPa	弹性模量 增幅/%
0	2.074	—	0.403	—
15	2.519	21.5	0.475	17.9
30	2.911	40.4	0.484	20.1
45	3.470	67.4	0.538	33.5
60	4.252	105.0	0.621	54.1

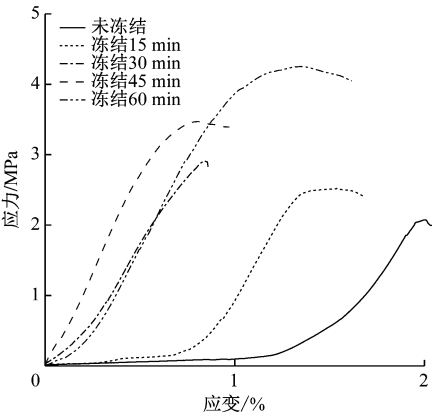


图 4 不同冻结时间下煤样应力-应变曲线

Fig. 4 Stress-strain curves of coal samples under different freezing time

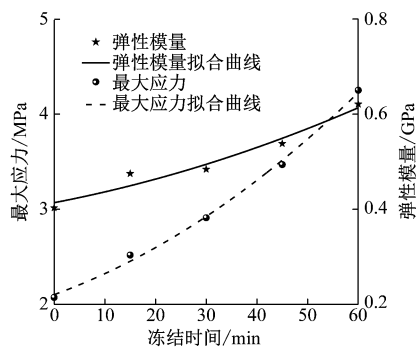


图5 不同冻结时间下煤样最大应力和弹性模量变化曲线
Fig. 5 Variation curves of maximum stress and elastic modulus of coal samples under different freezing time

3 结论

- (1) 随着冻结时间的增加,煤样内部及表面温度呈下降趋势;煤样表面最低温度位于 U 形铜管附近,煤样表面最高温度位于煤样边界。
- (2) 煤体在整个单轴压缩过程中依次经历压密、弹性变形、屈服和破坏 4 个阶段。在压密阶段,随着冻结时间的增加,煤样应变逐渐减小,压密阶段缩短;在弹性变形阶段和屈服阶段,随着冻结时间的增加,煤样最大应力和弹性模量均呈增大趋势。

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